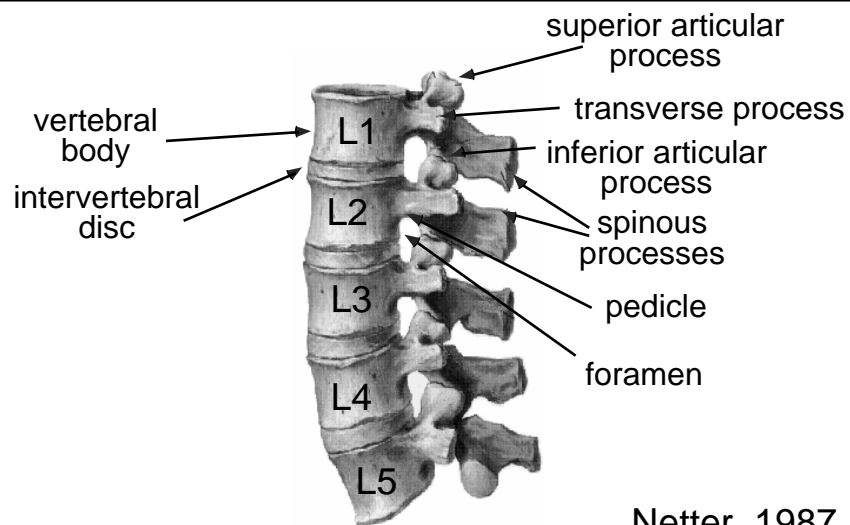
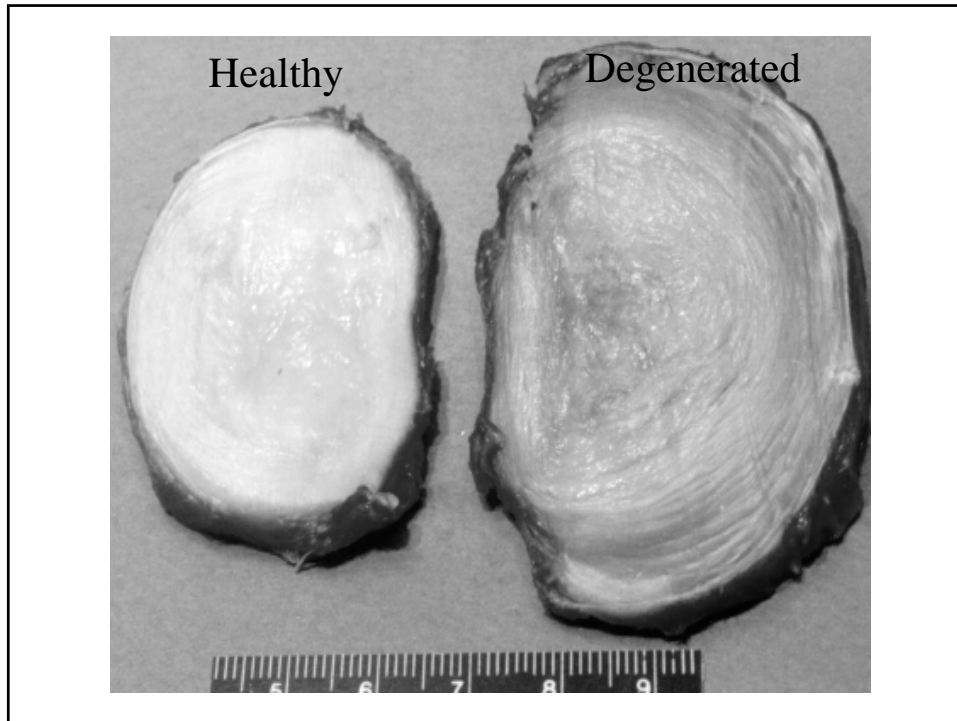


# Linear Viscoelasticity and the Relaxation Spectrum

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School of Engineering  
UVM

## Lumbar Spine





## Viscoelasticity

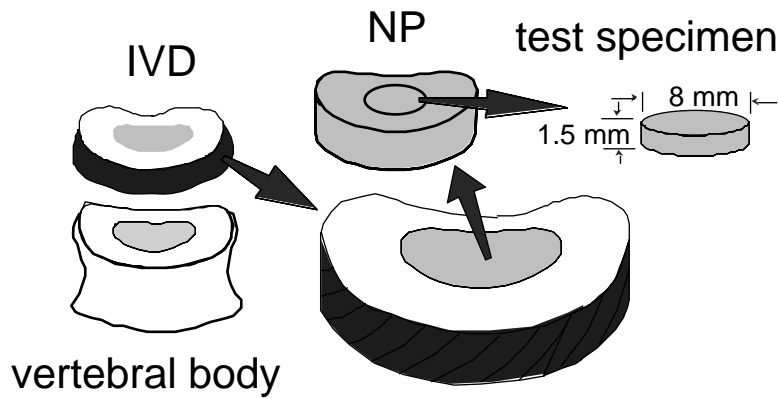
- Our bodies are mostly water
  - it just makes sense that water affects the mechanical behavior of biological soft-tissues
- Viscoelasticity
  - Flow independent viscoelasticity
    - polymeric matrix molecules reorient ... at their own pace
    - No volume changes
  - Flow dependent (Biphasic) viscoelasticity:
    - Water is forced out of the tissue like a sponge
    - Very small pores so this takes time
    - Requires volume changes

# The Viscoelastic Shear Behavior of the Human Lumbar Nucleus Pulposus

## Objectives

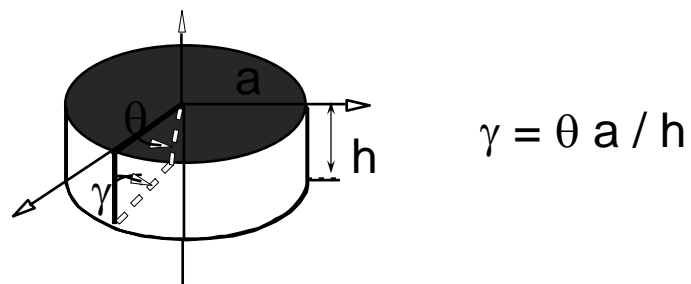
- Study the intrinsic viscoelastic behavior of the NP in shear
- Determine a constitutive relationship capable of describing this viscoelastic behavior

## Specimen Preparation



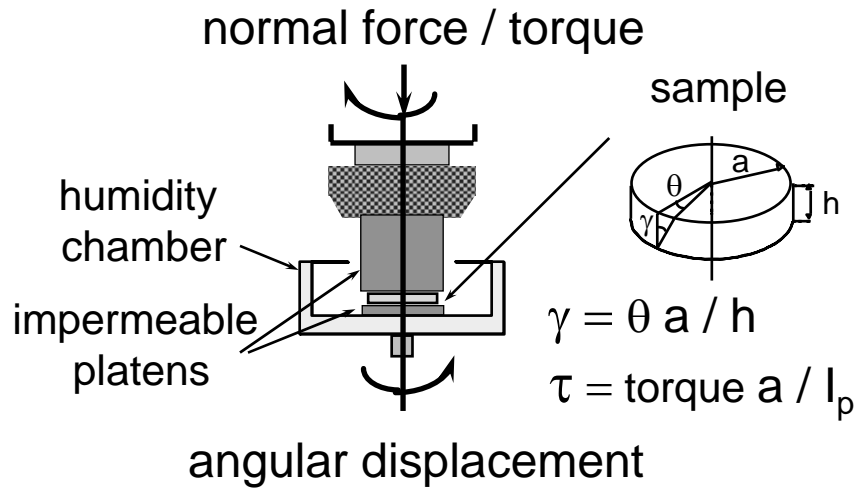
## Mechanical Testing

- Torsional shear strain ( $\gamma$ )



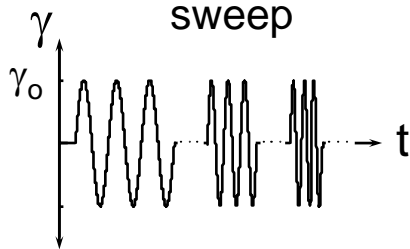
- No volumetric changes -->  
Negligible flow-dependent effects

# Shear Testing Apparatus



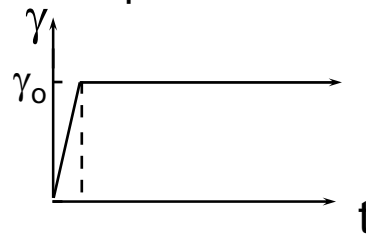
# Shear Testing Protocol

dynamic frequency sweep



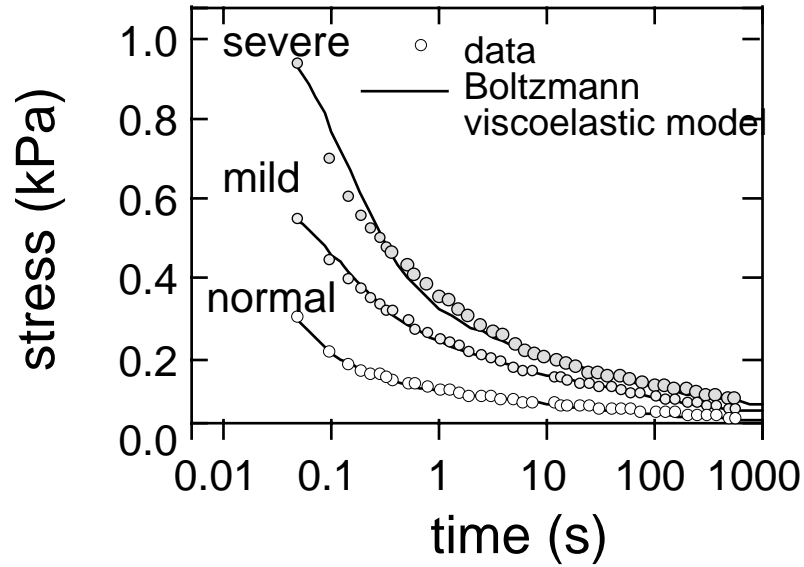
$\gamma_0 = 0.01 \text{ rad}$   
 $1 < \omega < 100 \text{ rad/s}$

stress relaxation experiments



3 tests @  $\gamma_0 = 0.05, 0.10, \text{ and } 0.15 \text{ rad}$

## Stress-Relaxation Experiment



Viscoelastic modeling

## Elastic Solid & Viscous Fluid

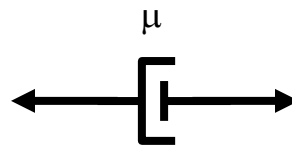
- Elastic solid

$$\tau = G\gamma$$



- Viscous fluid

$$\tau = \mu \dot{\gamma}$$

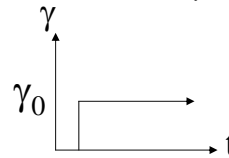
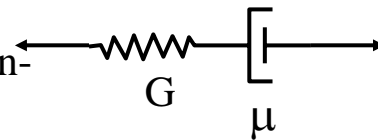


## Viscoelastic Models Maxwell Fluid: 2 constants

- Stress is a function of strain-rate

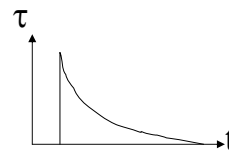
$$\tau + \lambda \dot{\tau} = \mu \dot{\gamma}$$

where  $\lambda = \mu/G$  and is the time constant



- Stress -relaxation function

$$\tau(t)/\gamma_0 = G(t) = (\mu/\lambda)\exp(-t/\lambda)$$



Relaxation function defined by viscosity  $\mu$  and relaxation time  $\lambda$

### 3 parameter solid

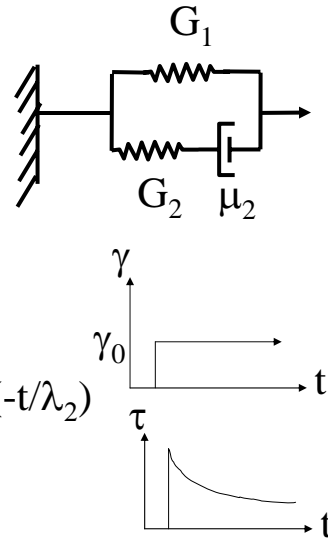
- Stress is a function of strain and strain-rate

$$\lambda_2 \dot{\tau} + \tau = (\mu_2 + \lambda_2 G_1) \dot{\gamma} + G_1 \gamma$$

- Relaxation Function

$$\tau(t)/\gamma_0 = G(t) = G_1 + (\mu_2/\lambda_2)\exp(-t/\lambda_2)$$

The relaxation function is defined by a single time constant,  $\lambda = \mu/G$

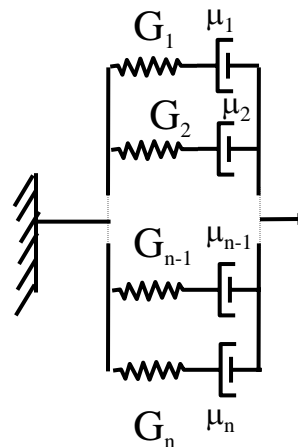


### Generalized Maxwell Model 2\*n parameters

- Consists of 'n' Maxwell units in parallel
- Stress -relaxation function

$$G(t) = \sum (\mu_i/\lambda_i)\exp(-t/\lambda_i)$$

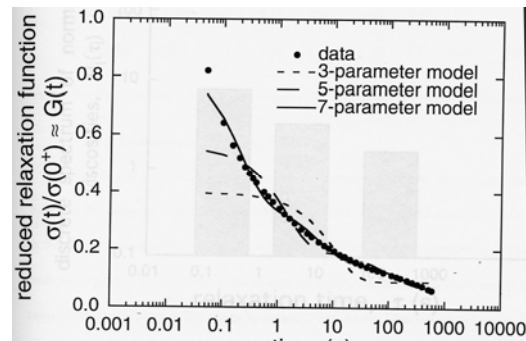
A relaxation function with DISCRETE relaxation times!



## Experimental data for human nucleus pulposus

- Curve fit with generalized maxwell model to obtain magnitudes of the time constants

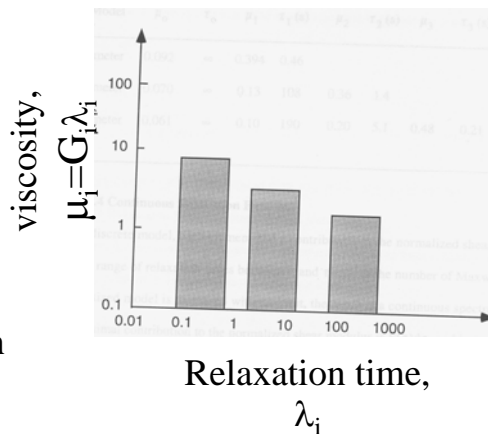
Good description of behavior!



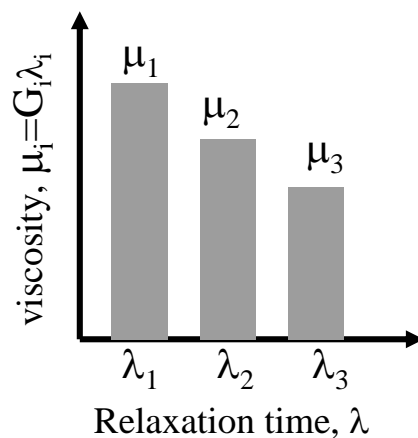
## Discrete relaxation spectrum

- 7 material parameters
  - 3 viscosities
  - 3 time constants
  - 1 equilibrium shear modulus
- Each bar corresponds to a single relaxation time and viscosity
- Note that amplitude of viscosities decrease with relaxation time

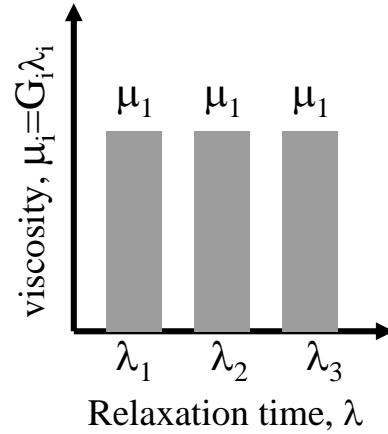
Relaxation spectrum  
(only shows 6 parameters)



## Discrete relaxation spectrum (2)



viscosities vary with relaxation time, 6 parameters needed

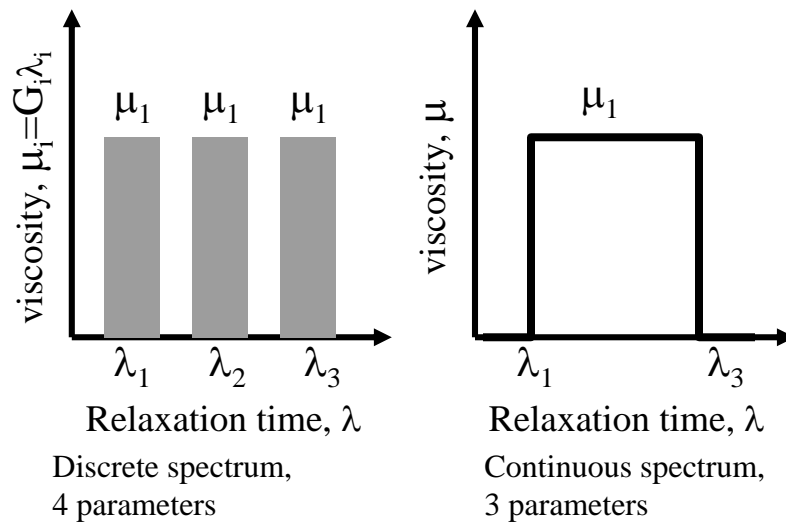


viscosities constant with relaxation time, 4 parameters needed

## Discrete relaxation spectrum (3)

- If a material has viscosities that are not a function of relaxation time, it is called a strain rate insensitive material
- If a material has viscosities that are a function of relaxation time, it is called a strain rate sensitive material

## Discrete & Continuous Relaxation Spectra



## Continuous Relaxation function

- An integral formulation for a continuous spectrum of relaxation times with constant amplitude

$$G(t) = 1 + \int_0^{\infty} S(t') \exp(-t/t') dt'$$

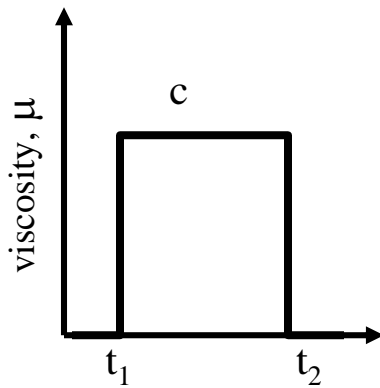
$$S(t) = \begin{cases} c/t & t_1 < t < t_2 \\ 0 & \text{otherwise} \end{cases}$$

Fung, 1981

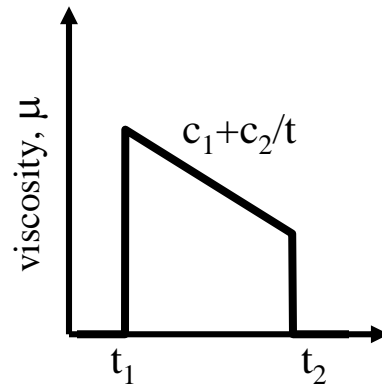
Only 3 constants:  $c$ ,  $t_1$ ,  $t_2$

these are similar to  $\mu_1$ ,  $\lambda_1$  and  $\lambda_3$

## Continuous Relaxation Spectra



Relaxation time,  $t$   
Continuous spectrum,  
3 parameters



Relaxation time,  $t$   
Continuous spectrum,  
4 parameters

## Continuous relaxation spectrum viscosities that decrease with relaxation time

Integral formulation with viscosities that decrease with relaxation time

$$G(t) = 1 + \int_0^{\infty} S(t') \exp(-t/t') dt' \quad \text{Fung, 1981}$$

Variable amplitude spectrum

$$S(t) = \begin{cases} (c_1 + c_2/t)/t & t_1 < t < t_2 \\ 0 & \text{otherwise} \end{cases}$$

latridis et al., 1997

## Reduced relaxation function

- Normalized by the value at  $t=0$
- For a discrete relaxation spectrum, we have:

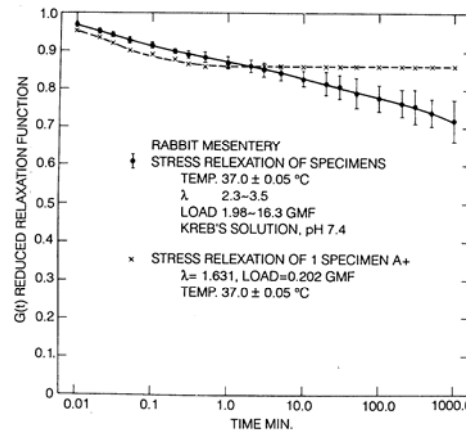
$$G(t) = \frac{\sum C_i e^{-t/\lambda_i}}{\sum C_i}$$

## Reduced relaxation function

- 2 important points
  - if an experiment is cut off prematurely, one may mistakenly arrive at the limiting value  $G(\infty)$ , corresponding to  $\lambda_i = \infty$
  - the relaxation times,  $\lambda_i$  should not be interpreted literally without realization that representation of empirical data by a sum of exponentials is a non-unique process

## Defining appropriate equilibrium time

- Stress relaxation for an individual specimen ended at 1min, however, for the average it went beyond 1000 min
- Fung, Fig7.5:4



## Non-uniqueness of exponentials

- These 3 exponentials all fit a certain set of experimental data equally well for x between 0 and 1. According to Lanczos (1956) and taken from Fung, p. 280.

$$f(x) = 2.202e^{-4.45x} + 0.305e^{-1.58x},$$

$$f(x) = 0.0951e^{-x} + 0.8607e^{-3x} + 1.5576e^{-5x},$$

$$f(x) = 0.041e^{-0.5x} + 0.79e^{-2.73x} + 1.68e^{-4.96x}.$$

## Reduced relaxation function with variable amplitude spectrum

### Reduced relaxation function

reduced means normalized by the value at t=0

$$G(t) = \frac{1 + \int_0^{\infty} S(t') \exp(-t/t') dt'}{1 + \int_0^{\infty} S(t') dt'} \quad \text{Fung, 1981}$$

### Variable amplitude spectrum

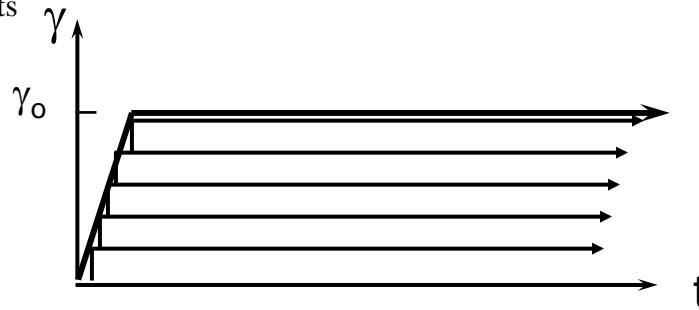
$$S(t) = \begin{cases} (c_1 + c_2/t)/t & t_1 < t < t_2 \\ 0 & \text{otherwise} \end{cases} \quad \text{Iatridis et al., 1997}$$

## Integral formulation for linear viscoelastic models

- Now that we know how to describe a step stress-relaxation experiment, we are ready to figure out how to describe any type of loading experiment

## Ramp stress-relaxation experiment

- A ramp stress relaxation experiment can be considered to be comprised of a series of infinitesimally small step stress relaxation experiments



- Any (displacement controlled) experiment can be considered to be comprised of a series of step stress relaxation summed together appropriately

## Boltzmann Linear Viscoelasticity Model (for stress response)

- Boltzmann superposition: Integral formulation for loading modes other than step strain input
- That is the superposition of infinite number of step stress relaxation experiments

$$\tau(t) = \int_{-\infty}^t G(t-t') G \frac{d\gamma}{dt'} dt'$$

$\tau(t)$  = shear stress

$\gamma(t)$  = shear strain

$G(t)$  = reduced relaxation function

$G$  = instantaneous shear modulus

## Boltzmann Linear viscoelasticity

- If the motion starts at  $t=0$  and  $\tau = \dot{\gamma} = 0$  for  $t < 0$ , we have the following (more practical) relationship:

$$\tau(t) = G(0)\dot{\gamma}(t) + \int_0^t \dot{G}(t')\dot{\gamma}(t-t')dt'$$

but  $G(0)=1$

- therefore, the shear stress at time  $t$  is equal to the instantaneous stress response decreased by an amount depending on the past history because  $dG/dt'$  is usually negative

## Boltzmann Linear Viscoelasticity Model (for strain response)

- Boltzmann superposition can also be used for creep responses.... That is the superposition of infinite number of step creep experiments

$$\tau(t) = \int_{-\infty}^t J(t-t') \dot{\gamma} dt'$$

$\tau(t)$  = shear stress

$\dot{\gamma}(t)$  = shear strain

$J(t)$  = reduced creep function

$J$  = instantaneous shear compliance

## Model predictions

- Use the Boltzmann linear viscoelasticity model (for stress response) with variable amplitude and continuous relaxation spectrum to describe and predict material behaviors

## Boltzmann Viscoelastic Law

$$\tau(t) = \int_{-\infty}^t G(t-t') \frac{d\gamma}{dt'} dt'$$

$\tau(t)$  = shear stress

$\gamma(t)$  = shear strain

$G(t)$  = reduced relaxation function

$\mu$  = instantaneous shear modulus

## Relaxation Function

Reduced relaxation function

$$G(t) = \frac{1 + \int_0^{\infty} S(t') \exp(-t/t') dt'}{1 + \int_0^{\infty} S(t') dt'} \quad \text{Fung, 1981}$$

Variable amplitude spectrum

$$S(t) = \begin{cases} c_1/t + c_2/t^2 & t_1 < t < t_2 \\ 0 & \text{otherwise} \end{cases}$$

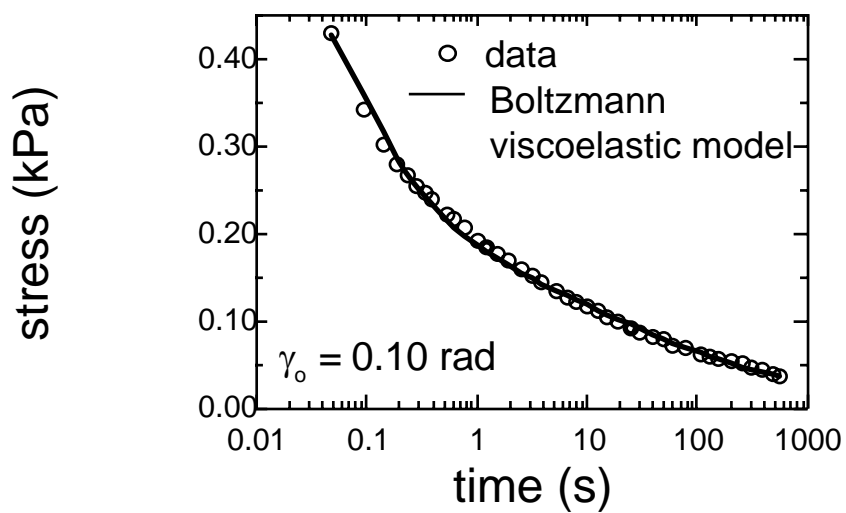
## Materials and Method

- 19 human lumbar discs (L2-5)  
average age 57 yrs (16-88 yrs)
- cylindrical NP specimens  
1.78 mm thick x 8.0 mm dia
- samples were prepared while frozen  
and tested in a humidity chamber

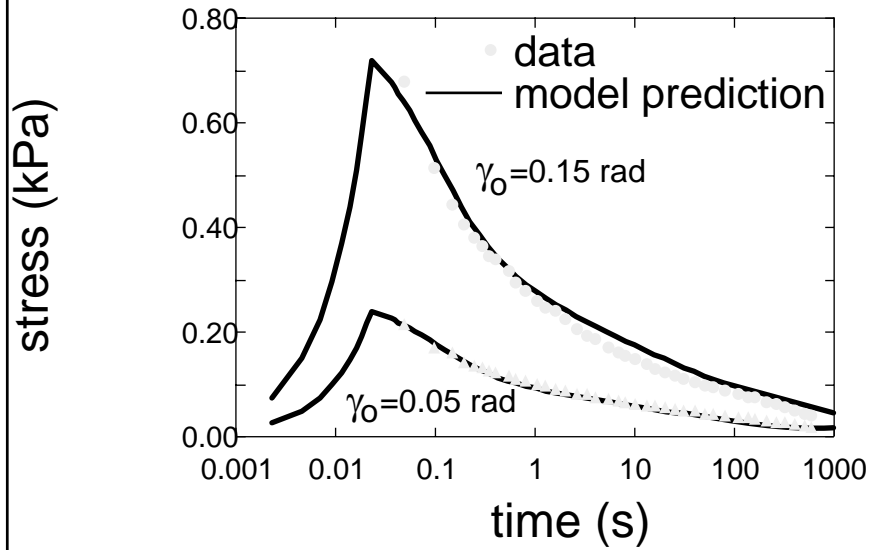
## Degenerative Level of NP

normal	mild	severe
grade I (n=7)	grade II-III (n=5)	grade IV-V (n=7)
gel-like blue-white	consolidation of fibrous tissue	clefts fissures

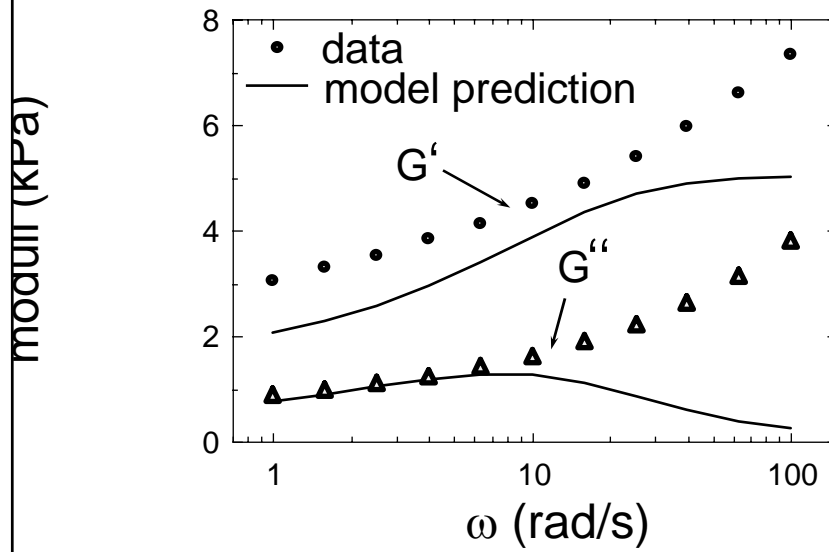
## Stress Relaxation



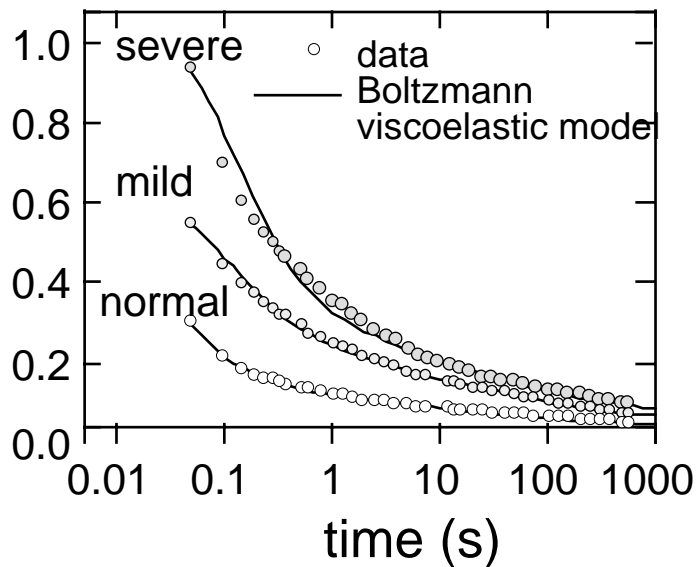
## Stress Relaxation



## Dynamic Frequency Sweep



## Stress-Relaxation Experiment

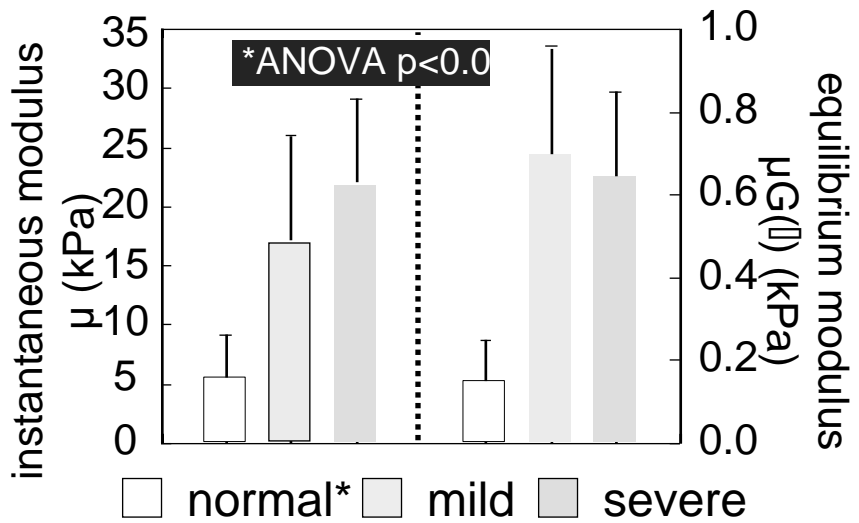


## Model Parameters

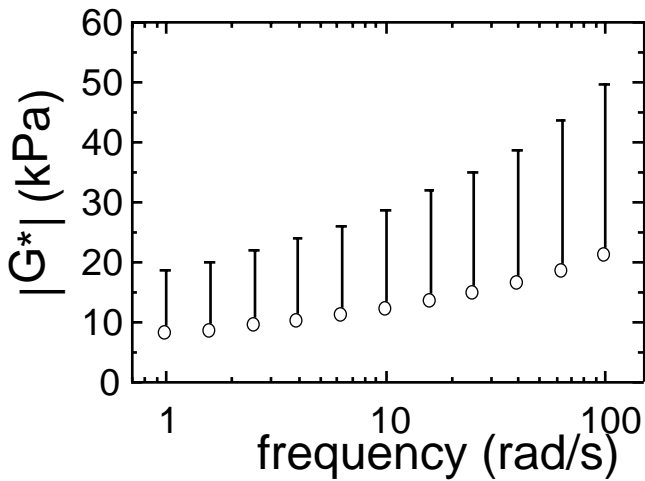
	normal	mild	severe
$\mu$ (kPa)*	$5.8 \pm 3.7$	$17.1 \pm 10.1$	$22.5 \pm 7.8$
$c_1$	$1.3 \pm 0.6$	$1.0 \pm 0.4$	$0.9 \pm 0.3$
$c_2$ (s)	$1.0 \pm 0.6$	$1.2 \pm 0.5$	$1.2 \pm 0.7$
$\tau_1$ (s)	$0.05 \pm 0.02$	$0.09 \pm 0.08$	$0.04 \pm 0.02$
$\tau_2$ (s)	600	600	600

\* significant effect of degeneration

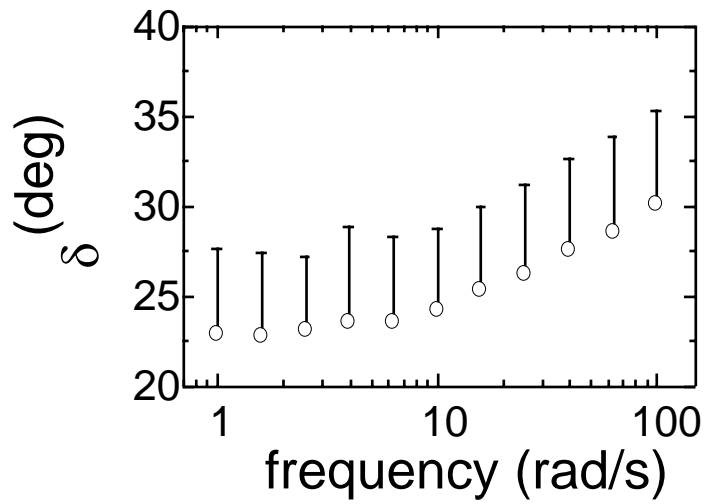
# Shear Moduli



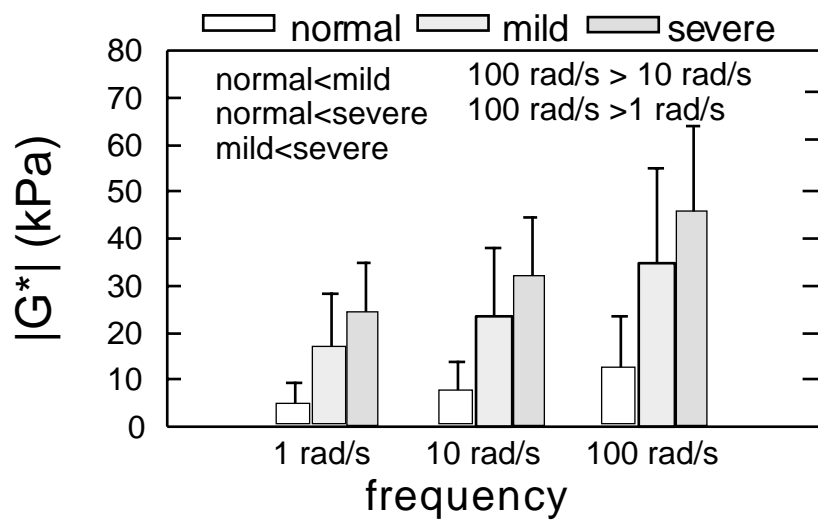
# Dynamic Frequency Sweep



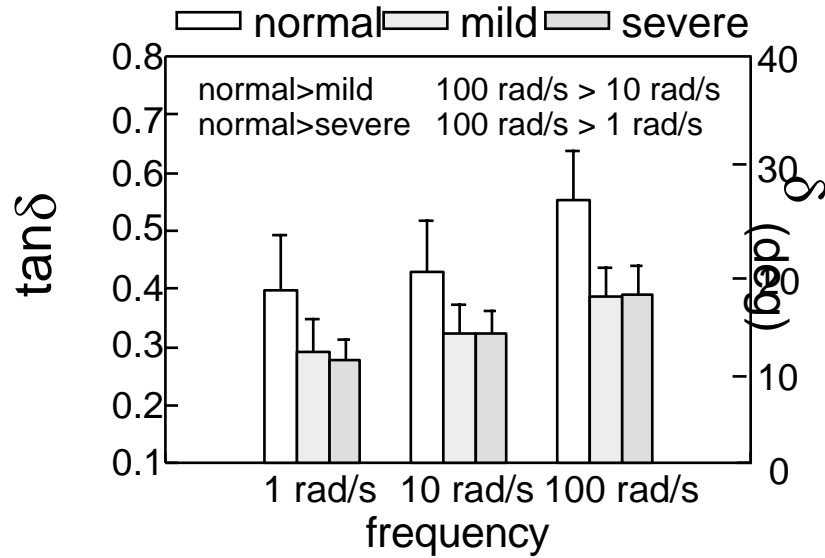
## Dynamic Frequency Sweep



## Dynamic Experiment



## Dynamic Experiment



## Dynamic Material Functions

	$ G^* $ (kPa)	$\delta$ (deg)	
articular cartilage	500	15	<div style="display: flex; align-items: center;"> <span style="font-size: 2em;">↓</span> </div>
meniscus	100	22	
degenerate NP	60	17	
normal NP	11	24	
proteoglycan solution	0.01	65	fluid

parameters determined @  $\omega = 10 \text{ rad / s}$

## Closure

This lecture summarized 3 major concepts:

- 1) The concept of relaxation spectrum and the pros/cons of choosing discrete vs continuous formulations. Note that the relaxation function is the solution for a step stress relaxation experiment.
- 2) The Boltzmann integral formulation for linear viscoelasticity was introduced and this was presented to provide a general way in which the relaxation function could be applied to general displacement control experiments, e.g., ramp stress relaxation and sinusoidal tests
- 3) One specific and somewhat complex form for linear viscoelastic model (i.e., the variable amplitude and continuous relaxation spectrum applied using the Boltzmann formulation for general loading conditions) was applied to the shear behaviors of human nucleus pulposus tissues.

## Future directions

- The next topic will be to next topic will be to expand on these concepts to analyze quasi-linear viscoelasticity and then to apply some of these concepts to experimental data.